# A Note on the Generalized Hohmann Transfer Time 

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We calculate the transfer time from the inner to the outer elliptic planetary orbits of a space vehicle for the four feasible configurations and for the circular case. We find that the least time of transfer $t_{T}$ corresponds to the second configuration.
Keywords: Astrodynamics, Hohmann transfer orbits.

## 1. Methods and Results

Generally the period of time spent in making the transfer from the inner planetary orbit to the outer one is given by [1]:

$$
\begin{equation*}
t_{T}=\pi\left[\frac{a_{T}^{3}}{\mu}\right]^{1 / 2} \tag{1}
\end{equation*}
$$

For circular inner and outer orbit case, we have:

$$
\begin{equation*}
a_{T}=\frac{a_{1}+a_{2}}{2} \tag{2}
\end{equation*}
$$

Where is the semi - major axis of the elliptic transfer orbit: $a_{1}, a_{2}$ are the two terminal orbits radii.

From previous literature of Kamel \& Soliman [2], we discover that there are four feasible configurations for the generalized Hohmann transfer.

For the first configuration (when the apo - apse of the transfer orbit coincides with the apo - apse of the final orbit) $a_{T}$ is given by:

$$
\begin{equation*}
a_{T}=\frac{a_{1}\left(1-e_{1}\right)+a_{2}\left(1+e_{2}\right)}{2} \tag{3}
\end{equation*}
$$

For the second configuration (when the apo - apse of the transfer orbit coincides with the peri - apse of the final orbit) ; third configuration (when the peri - apse of the transfer orbit coincides with the peri - apse of the final orbit) and fourth configuration (when the apo - apse of the transfer orbit coincides with the apo apse of the final orbit), we have respectively:

$$
\begin{align*}
& a_{T}=\frac{a_{1}\left(1-e_{1}\right)+a_{2}\left(1-e_{2}\right)}{2}  \tag{4}\\
& a_{T}=\frac{a_{1}\left(1+e_{1}\right)+a_{2}\left(1-e_{2}\right)}{2}  \tag{5}\\
& a_{T}=\frac{a_{1}\left(1+e_{1}\right)+a_{2}\left(1+e_{2}\right)}{2} \tag{6}
\end{align*}
$$

After little reduction, we get for the four configurations, successively:

$$
\begin{align*}
& t_{T}=\frac{\pi}{\sqrt{8 \mu}}\left[a_{1}\left(1-e_{1}\right)+a_{2}\left(1+e_{1}\right)\right]^{3 / 2}  \tag{7}\\
& t_{T}=\frac{\pi}{\sqrt{8 \mu}}\left[a_{1}\left(1-e_{1}\right)+a_{2}\left(1-e_{1}\right)\right]^{3 / 2}  \tag{8}\\
& t_{T}=\frac{\pi}{\sqrt{8 \mu}}\left[a_{1}\left(1+e_{1}\right)+a_{2}\left(1-e_{1}\right)\right]^{3 / 2}  \tag{9}\\
& t_{T}=\frac{\pi}{\sqrt{8 \mu}}\left[a_{1}\left(1+e_{1}\right)+a_{2}\left(1+e_{1}\right)\right]^{3 / 2} \tag{10}
\end{align*}
$$

Eqs (2), (7-10) show that we acquire different results for the different configurations, and also we get a different result when we compare the time of the elliptic terminal orbits with the circular terminal ones, since from Eqs (1), (2) where $e_{1}=$ $0, e_{2}=0$, we may write for the fifth configuration

$$
\begin{equation*}
t_{T}=\frac{\pi}{\sqrt{8 \mu}}\left[a_{1}+a_{2}\right]^{3 / 2} \tag{11}
\end{equation*}
$$

For the case of Earth - Mars transfer, we calculated the value of $t_{T}$ for the five configurations, where $\mu$ is the product of the Sun's mass and the gravitational constant. We may $\mu=1$ assume for analytical developments, and $a_{1}, a_{2}$ are the semi - major axes of the Earth and Mars respectively, whilst $e_{1}, e_{2}$ are the eccentricities of the Earth and Mars.

The calculations indicate that the least value of $t_{T}$ corresponds to the second configuration.

For the case of Earth - Mars transfer, we have:

$$
a_{1}=1 ; a_{2}=1.5237 ; e_{1}=0.0167 ; e_{2}=0.0934[3]
$$

| Fig | Eq. | $t_{T}$ |
| :--- | :--- | :--- |
| 1 | $(7)$ | 4.7896 |
| 2 | $(8)$ | 4.0389 |
| 3 | $(9)$ | 4.1248 |
| 4 | $(10)$ | 4.8805 |
| Circle | $(11)$ | 4.4531 |

## References

[1] Roy, A. E.: Orbital Motion, Fourth Edition, IOP publication Ltd., Bristol and Philadelphia, 2005.
[2] Kamel, O. M. and Soliman, A. S.: Mechanics and Mechanical Engineering, Lodz University of Technology, Poland, vol. 14 No. 1, $105-117,2010$.
[3] Murray, C. D. and Dermott, S. F.: Solar System Dynamics, Cambridge University Press, 1999.

